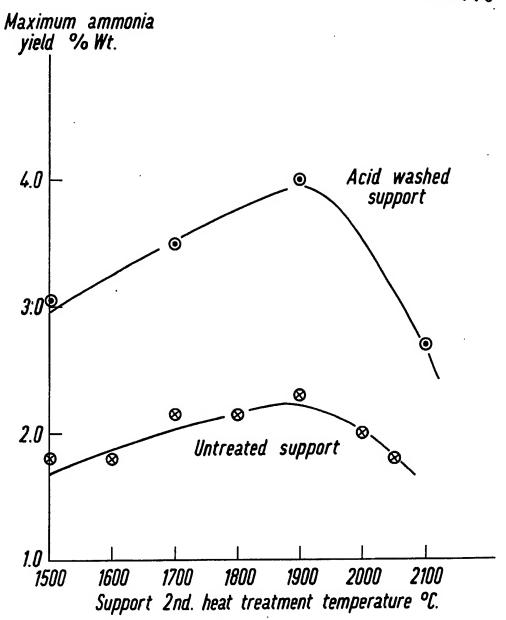
(12) UK Patent Application (19) GB (11) 2033776 A

- (21) Application No 7936642
- (22) Date of filing 23 Oct 1979
- (30) Priority data
- (31) 78/41708
- (32) 24 Oct 1978
- (33) United Kingdom (GB)
- (43) Application published 29 May 1980
- (51) INT CL³ B01J 23/56 23/16 C01C 1/04
- (52) Domestic classification
 B1E 1163 1180 1221
 1223 1298 1315 1324
 1471 1500 1513 1634
 1701 1712 1714 1718
 1721 1725 1728 1729
 1734 1741 E
 C1A J210 J243 J270
 J271 J285 J5 J603
 J604 J605 J608 J631
 J632 J634 J660 J685
 J688 L1C1
- (56) Documents cited
 GB 1498572
 GB 1471233
 GB 1413687
 GB 1011432
 S Berkman, J C Morrell
 & G Egloff, Catalysis
 Reinhold Publishing
 Corp NY 1940 p457 cl
 29-37
- (58) Field of search B1E C1A
- (71) Applicant
 The British Petroleum
 Company Limited
 Britannic House
 Moor Lane
 London
 EC2Y 9BU
- (72) Inventors
 Peter Gordon James
 Stephen Robert
 Tennison
- (74) Agents M MacLeod

(64) Catalyst for the production of ammonia

(57) A catalyst is prepared which comprises a transition metal, e.g., ruthenium, and a modifying metal, e.g., an alkali metal supported on a graphite—containing carbon support having specified surface area properties which has been washed with a concentrated solution of a strong mineral acid and then with water before impregnation with the other components. It is suitable for use in the production of ammonia.



SPECIFICATION

Catalyst for the production of ammonia

		Catalyst for the production of allimonia	
	5	This invention relates to a catalyst suitable for the production of ammonia. With increased pressure on the world's food resources the demand for nitrogen-containing fertilisers based on ammonia has grown rapidly in recent years. Current Haber processes using	5
	10	nitrogen and hydrogen as feedstock generally use a potassium promoted iron catalyst, usually with other promoters such as alumina. These catalysts are reduced in situ from bulk iron oxides before use and operate under severe conditions, e.g., pressures of up to 300 bars and temperatures of 450°—500°C.	10
	15	The reaction $N_2 + 3H_2 \rightleftharpoons 2NH_3$ is highly exothermic and thus the equilibrium is moved to the right at lower temperatures. However, present day commercial catalysts are not sufficiently active at lower temperatures to enable the reaction to reach equilibrium within the short time the reactants are in contact with the catalyst. Activity increases with temperature and therefore a	15
	20	compromise has to be reached. Recently work by Aika et al, Journal of Catalysis, 27, 424—431 (1972), on the synthesis of ammonia discloses that synthesis over a ruthenium catalyst is promoted by the addition of an alkali metal, particularly when the ruthenium is supported by active carbon or alumina. Similarly, British Patent Specification 1367112 to Sagami Chemical Research Centre discloses a complex catalyst for ammonia synthesis which comprises (a) at least one alkali metal belonging to Group 1A of the Periodic Table, (b) at least one compound, preferably a halide,	20
	25	oxide or sulphide, of a transition metal selected from the group consisting of Group 4B, Group 5B, Group 6B, Group 7B and Group 8 of the Periodic Table and graphite. The Periodic Table referred to by Sagami is that given in the "Handbook of Chemistry", edited by Norbert Adolf Lange; McGraw-Hill, 1961; pages 56 to 57. The complex comprises an alkali metal as the electron donor, graphite as the electron acceptor	25
	30	and a transition metal compound. The alkali metal and the transition metal compound are present as intercalates in the graphite lattice. Aika and Sagami both disclose the use of free alkali metal or precursors thereof, such as azides, as electron donors. Our copending British Patent Application No. 45711/76 discloses a catalyst comprising (i) as	30
•	35	support a graphite-containing carbon having (a) a basal plane surface area of at least 100 m²/g, (b) a ratio of BET surface area to basal plane surface area of not more than 8:1, preferably not more than 5:1 and (c) a ratio of basal plane surface area to edge surface area of at least 2:1 and preferably at least 5:1 and (ii) as active component (a) 0.1 to 50% preferably 1–30%, most preferably 5—10% by weight of a transition metal of the 4th, 5th and 6th horizontal Periods of Groups VB, VIB, VIIB and VIII of the Periodic Table expressed as % by weight of total catalyst	35
	40	and (b) 0.1 to 4 times by weight of (a) of a modifying metal ion selected from Groups IA or IIA of the Periodic Table or the lanthanides or actinides, the modifying metal ion being actively associated with the transition metal rather than the support. Unless otherwise indicated the Periodic Table referred to in the present specification is the Periodic Table published on page B-4 of the Handbook of Chemistry and Physics, 57th Edition, 1976—1977, published by CRC Press, Cleveland, Ohio.	40
	45	Such a catalyst is suitable for the production of ammonia from hydrogen and nitrogen and the Fischer-Tropsch reaction. It is distinguished from the prior art in that it is neither an electron donor-acceptor complex	45
	50	nor is it an intercalate compound. The graphite-containing carbon may be prepared by the method disclosed in British Patent Specification 1468441 comprising the steps of (1) an initial heat treatment in an inert atmosphere at a temperature between 900° and 3300°C, (2) an oxidation stage at a temperature between 300° and 1200°C, and (3) a further heat treatment in an inert atmosphere at a temperature between 1000° and 3000°C, preferably between 1400° and 2100°C. The activated carbons used in the preparation of the support invariably contain significant	50
	55	levels of impurities that can be deposited in the pore mouths during heat treatment resulting in a reduction in the accessible surface area. During or after the preparation the support may also become contaminated with sulphur compounds which subsequently have a deactivating effect. We have now discovered that washing the support with acid either during the carbon preparation or prior to the addition of the catalytically active substances both removed the	55
	60	sulphur and improves the surface properties of the carbon, thus resulting in a more active catalyst. Thus according to the present invention there is provided a method for the preparation of a catalyst comprising (i) as support a graphite-containing carbon having (a) a basal plane surface area of at least 100 m ² /g, (b) a ratio of BET surface area to basal plane surface area of not	60
	65	more than 8:1, preferably not more than 5:1 and (c) a ratio of basal plane surface area to edge surface area of at least 2:1 and preferably, at least 5:1 and (ii) as active component (a) 0.1 to	65

2

5	50% preferably 1–30%, most preferably 5—10% by weight of a transition metal of the 4th, 5th and 6th horizontal Periods of Groups VB, VIB, VIIB and VIII of the Periodic Table, expressed as % by weight of total catalyst and (b) 0.1 to 4 times by weight of (a) of a modifying metal ion selected from Groups IA or IIA of the Periodic Table or the lanthanides or actinides, the modifying metal ion being actively associated with the transition metal rather than the support, which method includes the steps of washing the carbon with a concentrated solution of a strong mineral acid, washing the acid treated carbon with water to remove the acid, then impregnating with a solution of a compound of the transition metal to give the desired concentration and							
10	with a solution of a compound of the transition metal to give the desired concentration and adding a solution of the Groups 1A, 2A, lanthanide or actinide compound to give the desired 10 concentration of the modifying metal ion. If the graphite containing carbon is prepared by the method of 1468441, then the acid was may take place either before the first heat treatment, between the first and second heat treatments or after the final heat treatment.							
15	The preferred transition metals are cobalt, ruthenium and rhodium. Ruthenium is the most preferred.							
	rubidium and potassium.	(b) are the alkali and alkaline earth metal ions. The most preferred are						
20	first.		ric, nitric and sulphuric acids, preferably the	20				
20	According to another aspect of the present invention, there is provided a process for the production of ammonia which process comprises passing a feedstock containing nitrogen and hydrogen over a catalyst prepared as herein before described under conditions of temperature,							
25	pressure and space velocity such that conversion to ammonia is effected. Synthesis gas is a suitable feedstock. The Catalyst has a high tolerance of poisons which are normally harmful to conventional catalysts, such as water and carbon monoxide. Broad and preferred ranges of process conditions are as follows:							
30		process condition	is are as runows.	30				
-	Broad F	Range	Preferred Range					
35	Temperature °C 250-6 Pressure bars Atmosp		300-500 20-200 5,000—30,000	35				
		The invention is illustrated by the following example and the accompanying drawing.						
40	The invention is illustrated by the	he following exa	mple and the accompanying drawing.	40				
	Example Activated carbon AC 40 supplies the heat treatment continued to 1 weight loss. Portions of the oxidis temperatures ranging from 1500	ed by CECA Limi 500°C in argon. ed material were	mple and the accompanying drawing. ted was heat treated to 900°C in nitrogen and It was then oxidised in air at 450°C to 20% then heat treated in argon at various rm graphite-containing carbon catalyst	45				
45	Example Activated carbon AC 40 supplies the heat treatment continued to 1 weight loss. Portions of the oxidis temperatures ranging from 1500 supports. Samples of the latter were then distilled water until free from chlo	ed by CECA Limi 500°C in argon. ed material were to 2100°C to fo boiled in 40% I ride ions.	ted was heat treated to 900°C in nitrogen and It was then oxidised in air at 450°C to 20% then heat treated in argon at various rm graphite-containing carbon catalyst HCI and subsequently Soxhlet extracted with	45 .				
	Example Activated carbon AC 40 supplies the heat treatment continued to 1 weight loss. Portions of the oxidis temperatures ranging from 1500 supports. Samples of the latter were then distilled water until free from chlocatalysts were prepared by add aqueous solution of ruthenium chrubidium was added from an aque	ed by CECA Limi 500°C in argon. ed material were to 2100°C to fo boiled in 40% I ride ions. ing 7.5% ruthen loride. After redu	ted was heat treated to 900°C in nitrogen and It was then oxidised in air at 450°C to 20% then heat treated in argon at various rm graphite-containing carbon catalyst HCI and subsequently Soxhlet extracted with nium to the supports by impregnation from an action at 500°C in hydrogen for 2 hours 15% rubidium nitrate. After a further heat treatment	45				
45	Example Activated carbon AC 40 supplies the heat treatment continued to 1 weight loss. Portions of the oxidis temperatures ranging from 1500 supports. Samples of the latter were then distilled water until free from chlocatalysts were prepared by add aqueous solution of ruthenium chrubidium was added from an aque at 500°C in nitrogen the catalysts. The catalysts were then tested is 5.14 bar. In each test the temper maximum ammonia yield noted.	ed by CECA Limito 500°C in argon. The sed material were to 2100°C to form boiled in 40% limits and in a 2 ml microre ature was programmed.	ted was heat treated to 900°C in nitrogen and It was then oxidised in air at 450°C to 20% of then heat treated in argon at various rm graphite-containing carbon catalyst HCl and subsequently Soxhlet extracted with nium to the supports by impregnation from an action at 500°C in hydrogen for 2 hours 15% rubidium nitrate. After a further heat treatment use. Pactor at a GHSV of 1000 and a pressure of immed over the range 350°—450°C and the	45 .				
45	Example Activated carbon AC 40 supplies the heat treatment continued to 1 weight loss. Portions of the oxidis temperatures ranging from 1500 supports. Samples of the latter were then distilled water until free from chlocatalysts were prepared by add aqueous solution of ruthenium chrubidium was added from an aque at 500°C in nitrogen the catalysts. The catalysts were then tested is 5.14 bar. In each test the temper maximum ammonia yield noted. The results obtained are plotted temperature of the second heat the	ed by CECA Limit 500°C in argon. The sed material were to 2100°C to form boiled in 40% in a 2 ml microre to 3 ml microre to 3 ml microre to 4 ml microre to 5	ted was heat treated to 900°C in nitrogen and It was then oxidised in air at 450°C to 20% of then heat treated in argon at various rm graphite-containing carbon catalyst. HCI and subsequently Soxhlet extracted with nium to the supports by impregnation from an action at 500°C in hydrogen for 2 hours 15% rubidium nitrate. After a further heat treatment use.	45 .				
45	Example Activated carbon AC 40 supplies the heat treatment continued to 1 weight loss. Portions of the oxidis temperatures ranging from 1500 supports. Samples of the latter were then distilled water until free from chlocatalysts were prepared by add aqueous solution of ruthenium chrubidium was added from an aque at 500°C in nitrogen the catalysts. The catalysts were then tested is 5.14 bar. In each test the temper maximum ammonia yield noted. The results obtained are plotted temperature of the second heat trammonia yield expressed as a per	ed by CECA Limit 500°C in argon. The sed material were to 2100°C to form boiled in 40% in a 2 ml microre to 3 ml microre to 3 ml microre to 4 ml microre to 5	ted was heat treated to 900°C in nitrogen and It was then oxidised in air at 450°C to 20% of then heat treated in argon at various rm graphite-containing carbon catalyst HCI and subsequently Soxhlet extracted with nium to the supports by impregnation from an action at 500°C in hydrogen for 2 hours 15% rubidium nitrate. After a further heat treatment use. Pactor at a GHSV of 1000 and a pressure of ammed over the range 350°—450°C and the anying drawing which is a graph in which the	45 .				

1. A method for the preparation of a catalyst comprising (i) as support a graphite-containing 65 carbon having (a) a basal plane surface area of at least 100 m²/g, (b) a ratio of BET surface

65

	area to basal plane surface area of not more than 8:1, and (c) a ratio of basal plane surface area to edge surface area of at least 2:1 and (ii) as active component (a) 0.1 to 50% by weight of a transition metal of the 4th, 5th and 6th horizontal Periods of Groups VB, VIB, VIIB and VIII of the Periodic Table, expressed as % by weight of total catalyst and (b) 0.1 to 4 times by weight	
5	of (a) of a modifying metal ion selected from Groups IA or IIA of the Periodic Table or the lanthanides or actinides, the modifying metal ion being actively associated with the transition metal rather than the support, which method includes the steps of washing the carbon with a concentrated solution of a strong mineral acid, washing the acid treated carbon with water to	5
10	remove the acid, then impregnating with a solution of a compound of the transition metal to give the desired concentration and adding a solution of the Groups IA, IIA, lanthanide or actinide compounds to give the desired concentration of the modifying metal ion. 2. A method according to Claim 1 wherein the graphite-containing carbon has a ratio of BET surface area to basal plane surface area of not more than 5:1 and a ratio of basal plane surface	10
15	area to edge surface area of at least 5:1. 3. A method according to either of Claims 1 or 2 wherein the transition metal is present in amount 1 to 30% by weight expressed as % by weight of total catalyst. 4. A method according to any of the preceding claims wherein the transition metal is ruthenium.	15
20	 5. A method according to any of the preceding claims wherein the modifying metal ions are rubidium or potassium ions. 6. A method according to any of the preceding claims wherein the strong mineral acid is hydrochloric acid. 	20
25	 A method according to any of the preceding claims wherein the concentration of the strong mineral acid lies in the range 10 to 80% by volume. A process for the production of ammonia which process comprises passing a feedstock containing nitrogen and hydrogen over a catalyst prepared as hereinbefore described under conditions of temperature, pressure and space velocity such that conversion to ammonia is effected. 	25
30	9. A process according to Claim 8 wherein the feedstock is passed over the catalyst at a temperature in the range 250° to 600°C, a pressure in the range atmospheric to 300 bars and a space velocity in the range 1,000 to 100,000 v/v/hr. 10. A process according to Claim 9 wherein the feedstock is passed over the catalyst at a temperature in the range 300° to 500°C, a pressure in the range 20 to 200 bars and a space	30
35	velocity in the range 5,000 to 30,000 v/v/hr. 11. A method for the preparation of a catalyst according to Claim 1 as hereinbefore described with reference to the Example. 12. A process for the production of ammonia as hereinbefore described with reference to the Example.	35
40	13. Catalysts whenever prepared by a method according to any of Claims 1 to 7 or 11.14. Ammonia whenever prepared by a process according to any of Claims 8 to 10 or 12.	40